
CrYogenic Brightness-Optimized Radiofrequency Gun (CYBORG) HG2022

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Outline of presentation



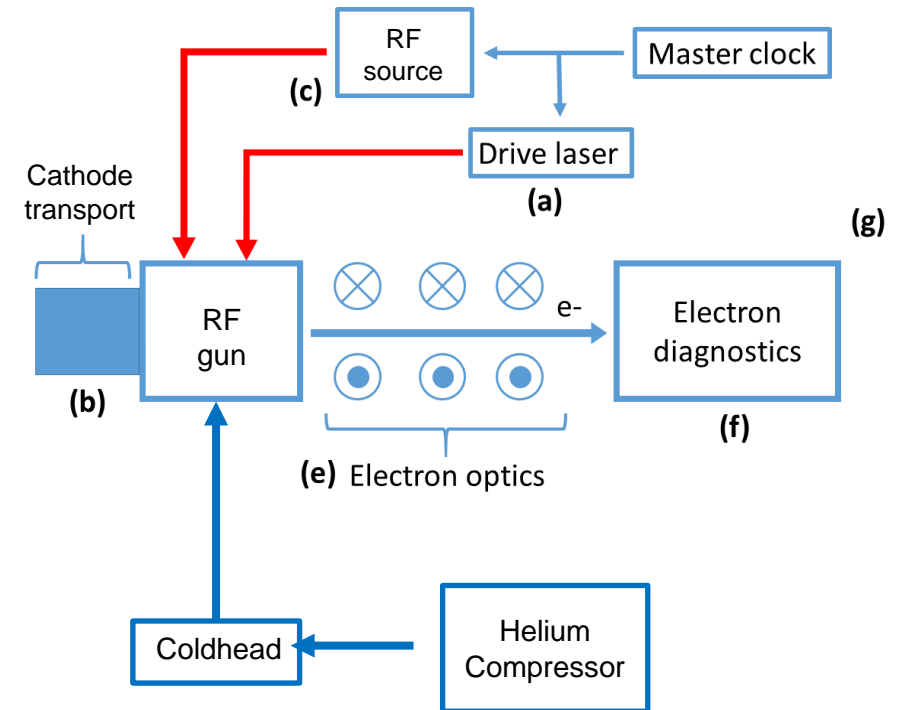
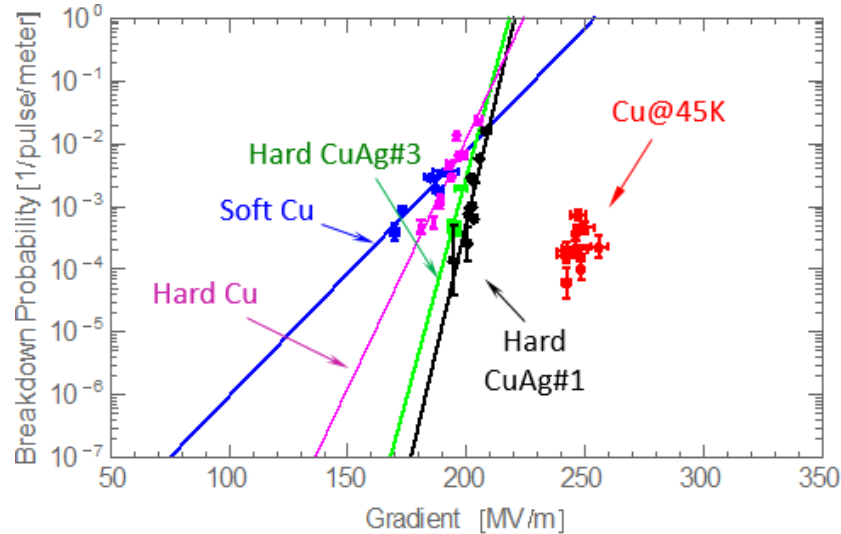
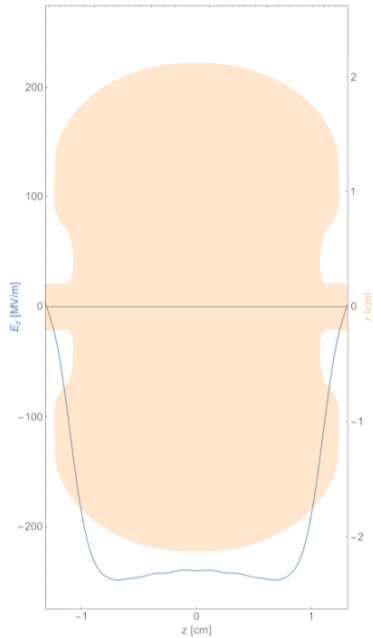
1. Background & motivations
2. CYBORG Design
3. Fabrication status & LLRF
4. Future Steps
5. Conclusions



1) CYBORG Functions



1. Cavity fabrication & structure test
2. Infrastructure development
3. Low temperature emission/photocathode test bed



RR Robles et al. *Physical Review Accelerators and Beams* 24 (6), 063401

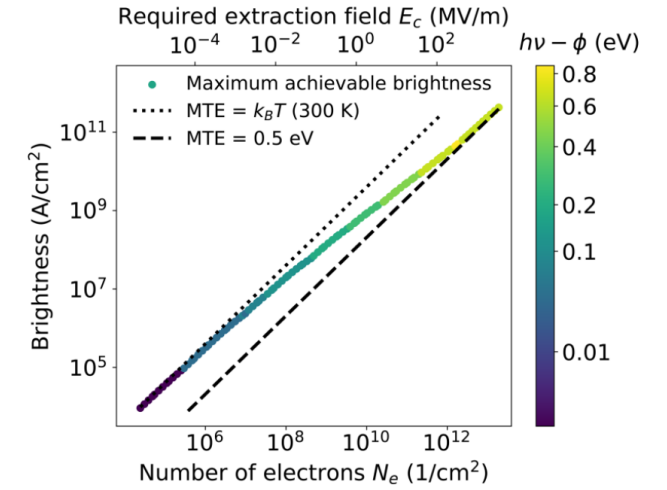
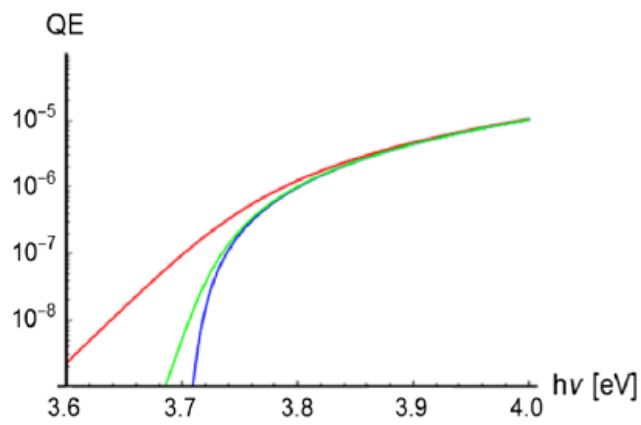
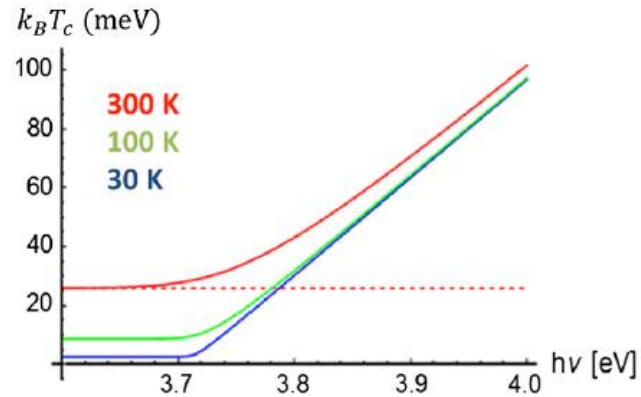


1) CYBORG Functions (2)

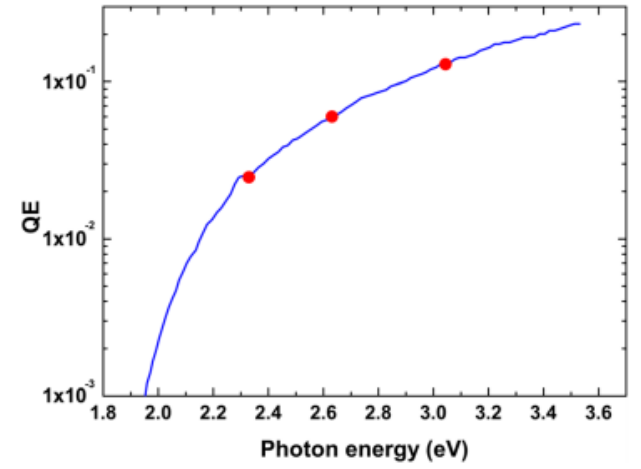


- Collaboration within NSF Center for Bright Beams
- Low temperature at increases launch field and decreases cathode mean transverse energy but also QE
- Test bed for cathodes cold & high field environment

$$B_{e,b} \approx \frac{2ec\epsilon_0}{k_B T_c} (E_0 \sin \varphi_0)^2$$



J. K. Bae, I. Bazarov, P. Musumeci, S. Karkare, H. Padmore, and J. Maxson, J. Appl. Phys. 124, 244903 (2018).

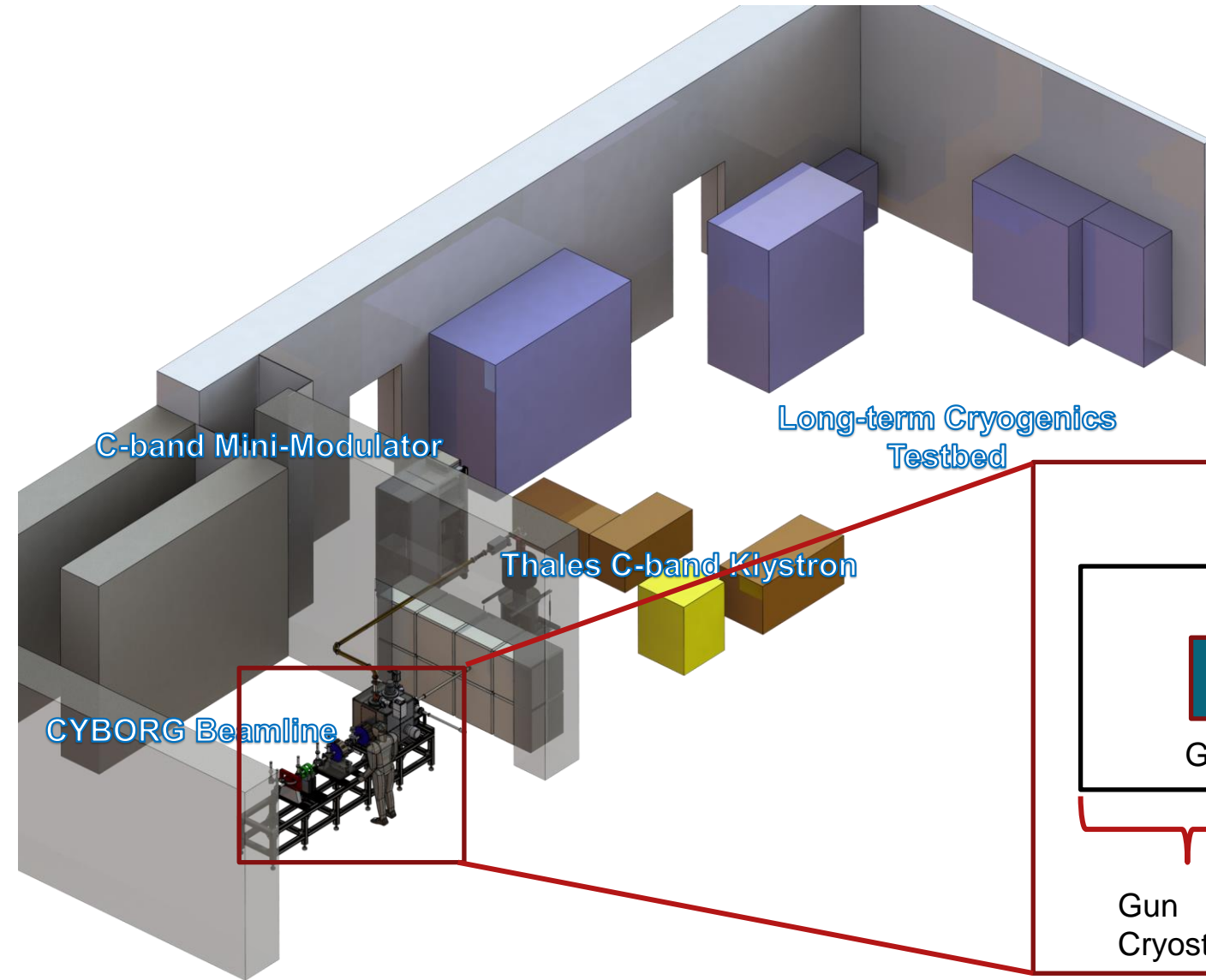


L. Cultrera et al., Appl. Phys. Lett. 103, 103504 (2013).

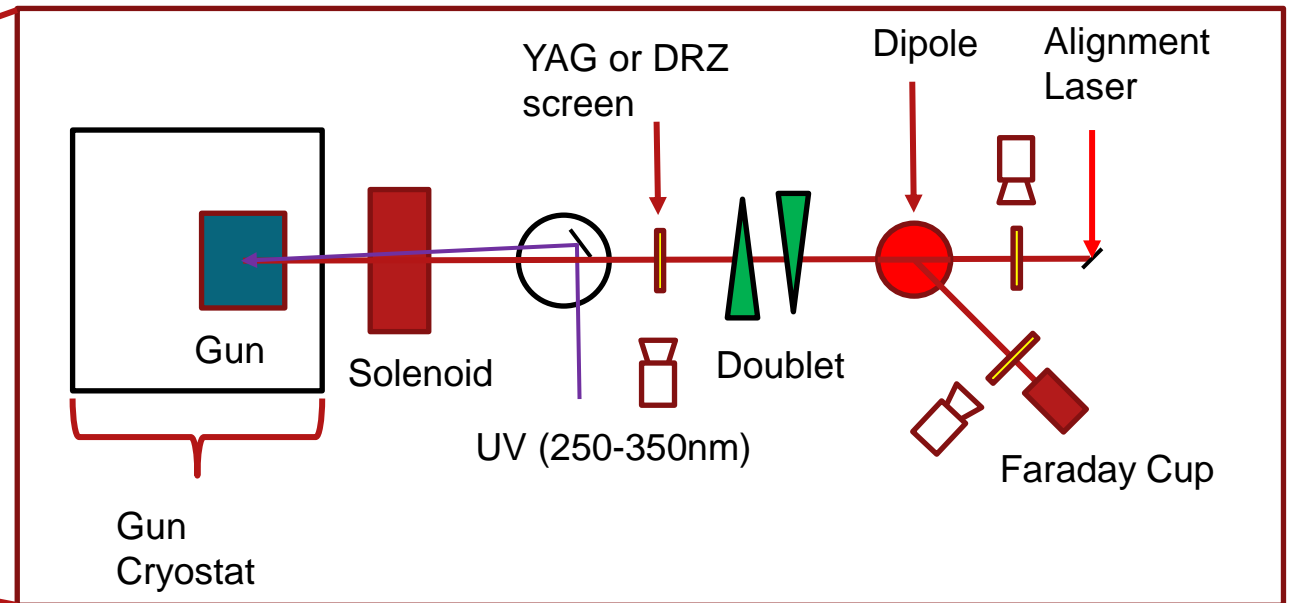


1) Beamline development phases

- Phase 1 = copper cathode
 - Config 1 = only gun
 - Config 2 = w/ beamline
- Phase 2 = high brightness cathode



Phase1:config2

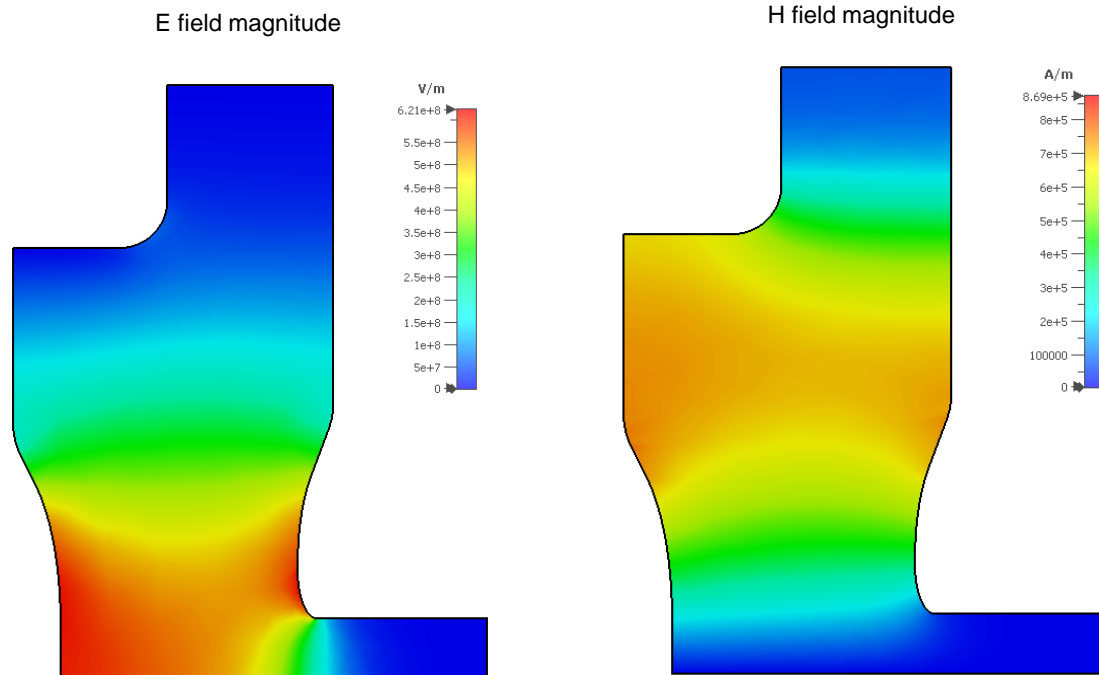




2) RF Design Parameters



- Reentrant cavity with high shunt impedance
- Peak electric field around cathode surface



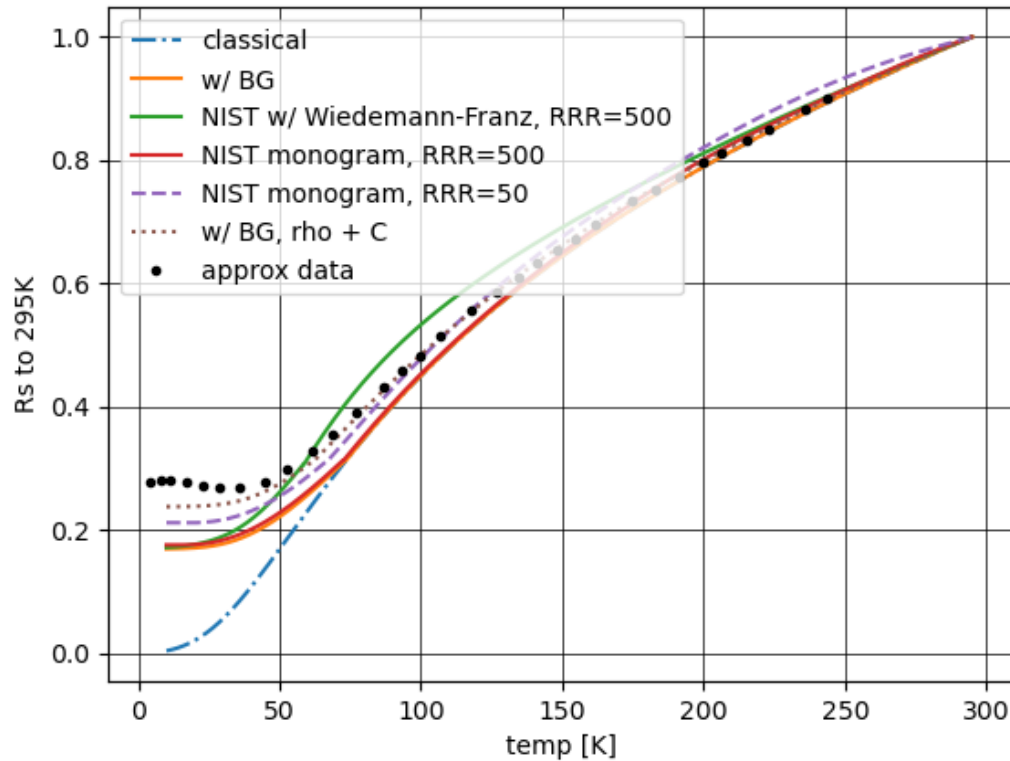
Parameter	295K	77K	45K
Launch field	-	120 MV/m	120 MV/m
Frequency	5.695 GHz	5.712 GHz	5.713 GHz
β	0.7	4	5.3
Q0	8579	23000	38000
Filling time	-	0.26 us	0.3 us
RF Power requirement	-	0.52 MW	0.48 MW
Energy deposition	-	0.17 J/pulse	0.1 J/pulse



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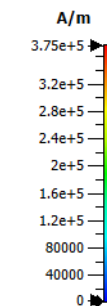
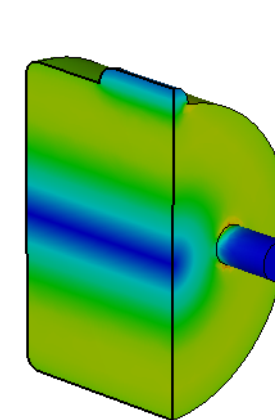
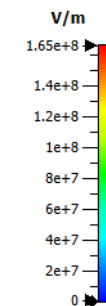
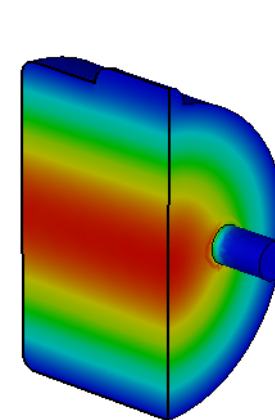
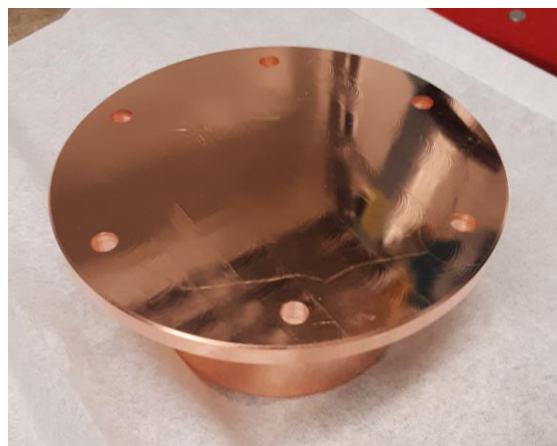
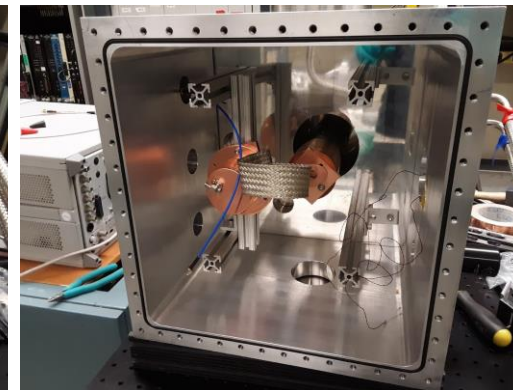
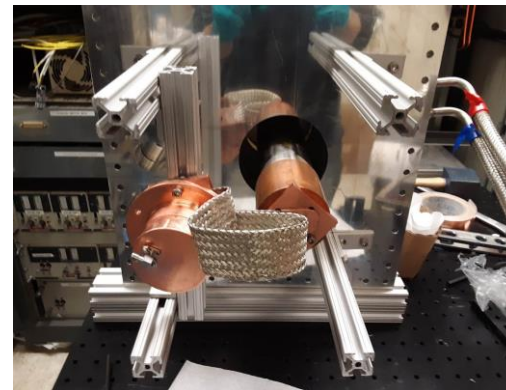
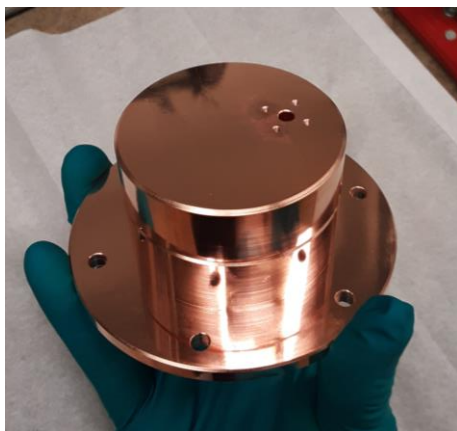
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3a) LLRF Measurements



- Copper pillbox cavities used for Cband low level LLRF

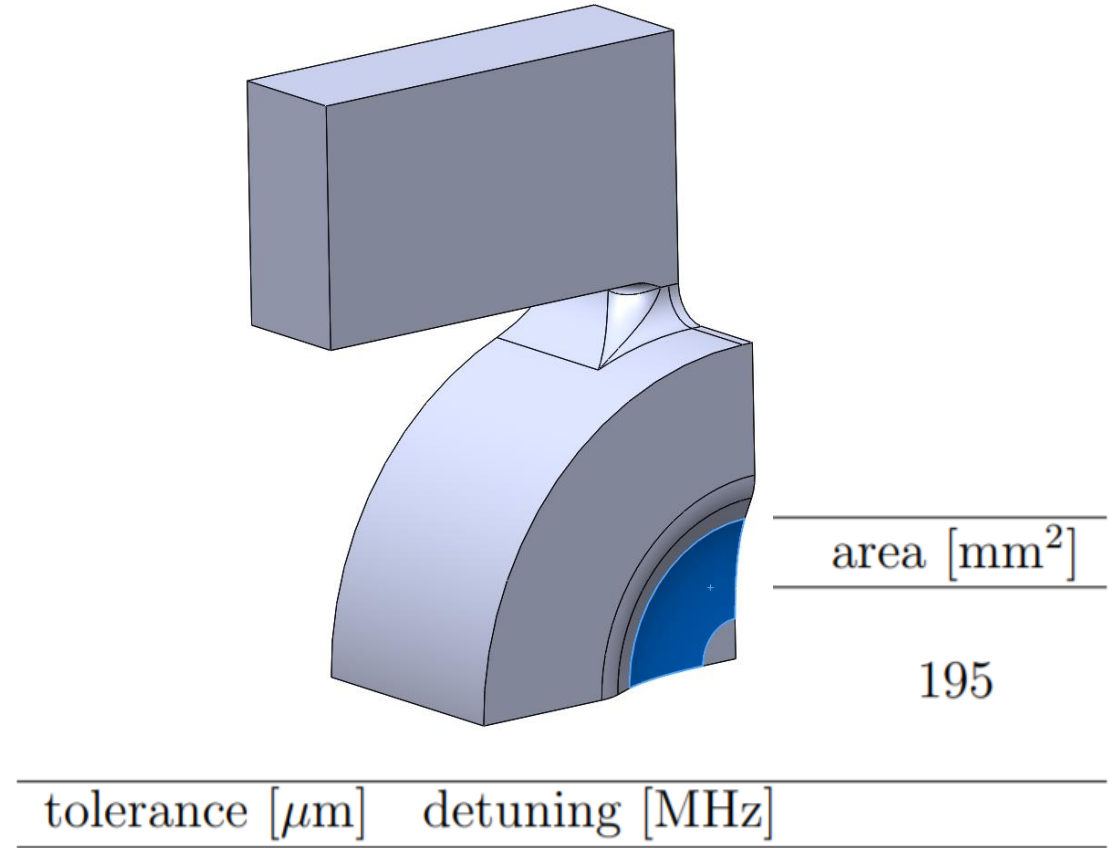
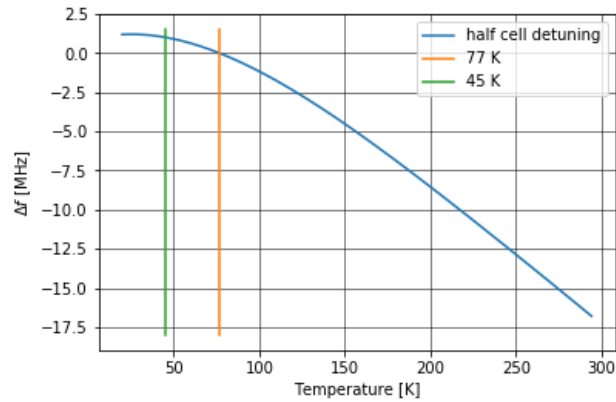




2) Surface Sensitivity



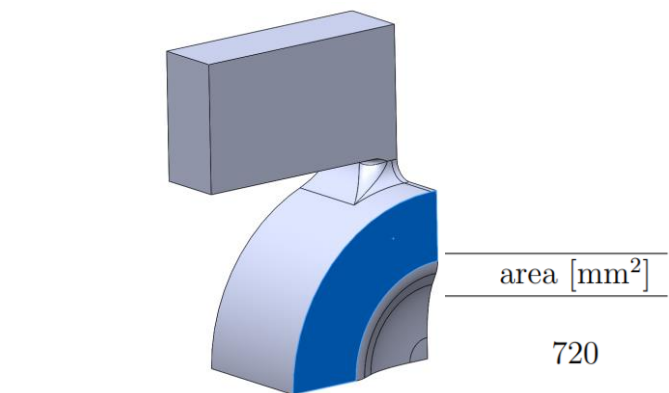
- Cryogenic temperature provides additional RF stability
- Slater perturbation theory gives frequency change from small displacement of one surface
- Default 10 um
- For surfaces of high field tolerance reduced to 5 um (detuning > ≈ |0.2| MHz w/ 10 um perturbation, most |10s| kHz)
- Adding in quadrature leads to 1.6 MHz from following



$$\Delta f_i = \Delta s_i \frac{f_0}{4U} \int_{S_i} (\mu |H_0|^2 - \epsilon |E_0|^2) dS$$

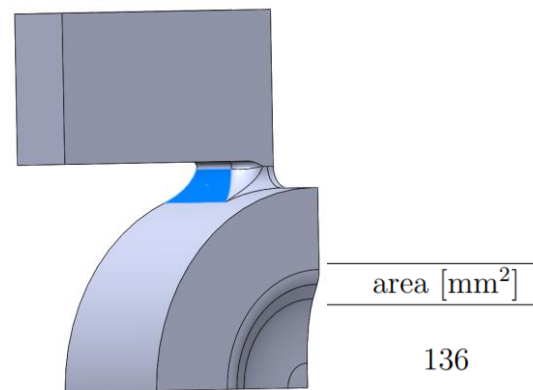


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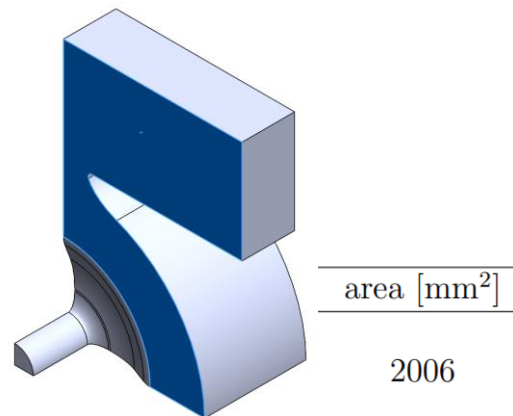
tolerance [μ m] detuning [MHz]

5 0.648



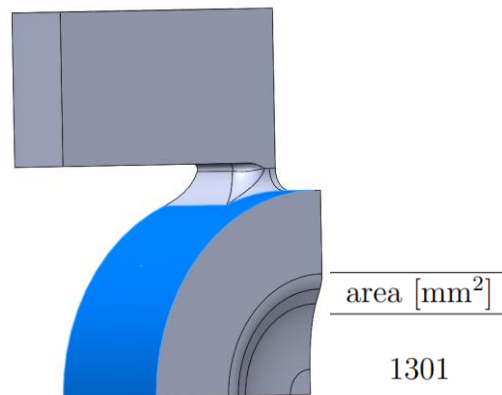
tolerance [μ m] detuning [MHz]

5 0.196



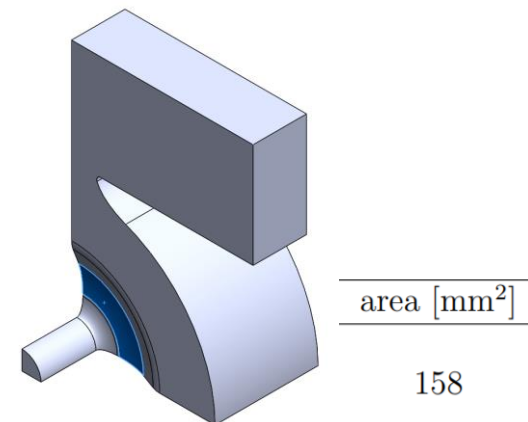
tolerance [μ m] detuning [MHz]

5 0.643



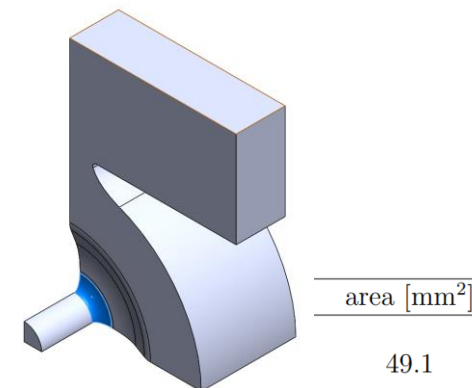
tolerance [μ m] detuning [MHz]

5 1.21



tolerance [μ m] detuning [MHz]

5 -0.533



tolerance [μ m] detuning [MHz]

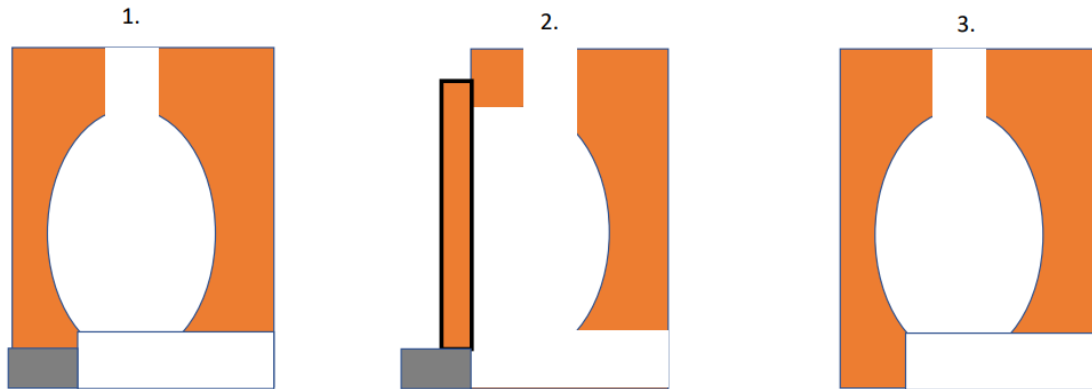
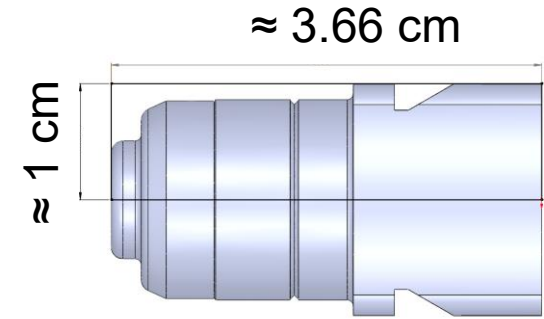
5 -0.261



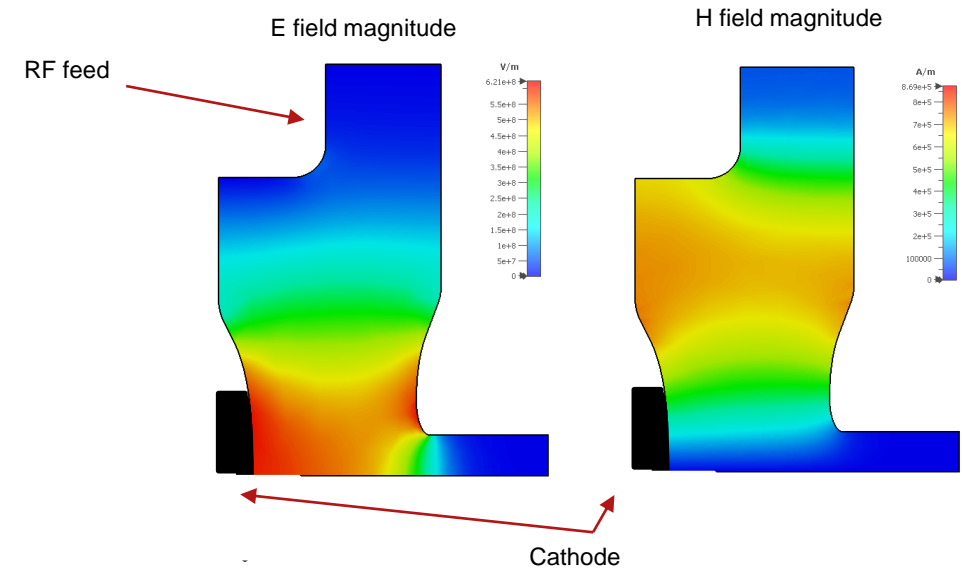
2) Cathode Interface



- Forward compatibility needed for INFN style mini puck, etc.
- For phase 1 of test bed, CF flange sealed off w/ blank from back of cavity and test copper cathode



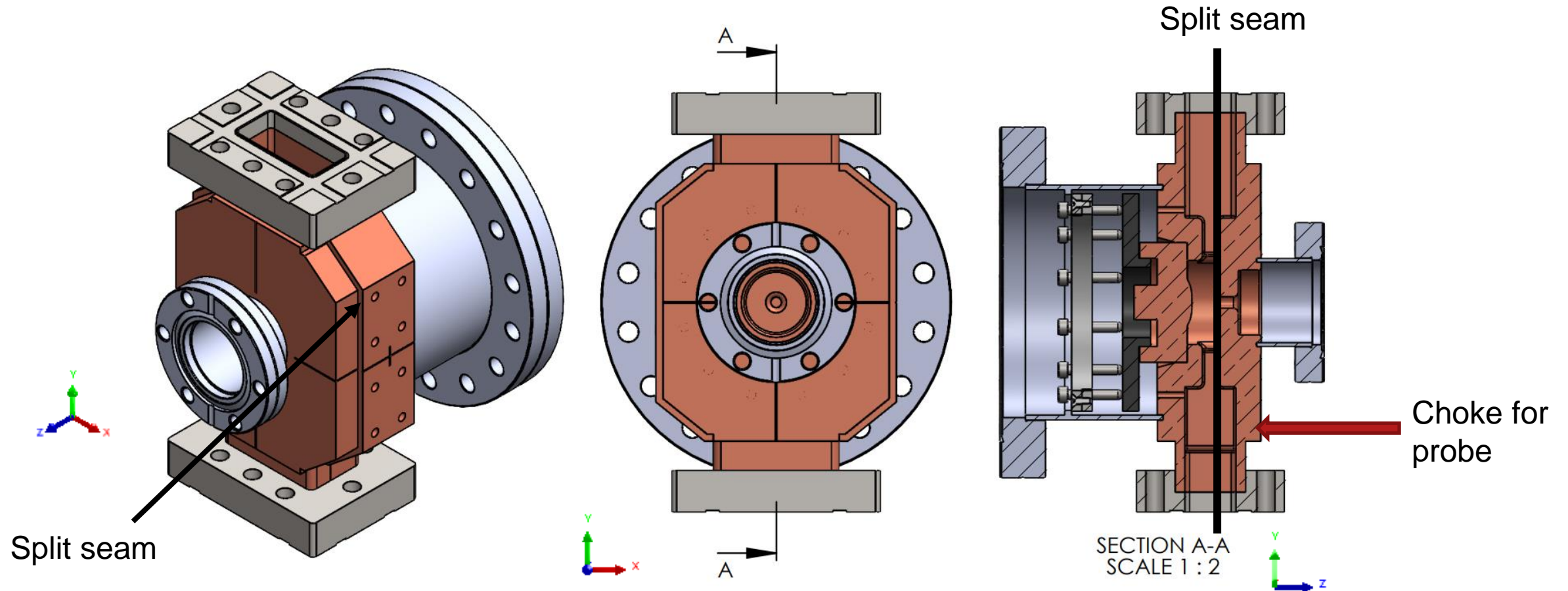
- Plug directly into cavity
- Useful for 1.6 cell to max gradient
- Good for cathode tests
- High gradient (120 MV/m) but lower than plug alone
- No cathode exchange
- Highest achievable gradients





2) Drawings

- Split seam for brazing necessitated by tolerance location
- Drawings with fully removable backplane based on FERMI gun design



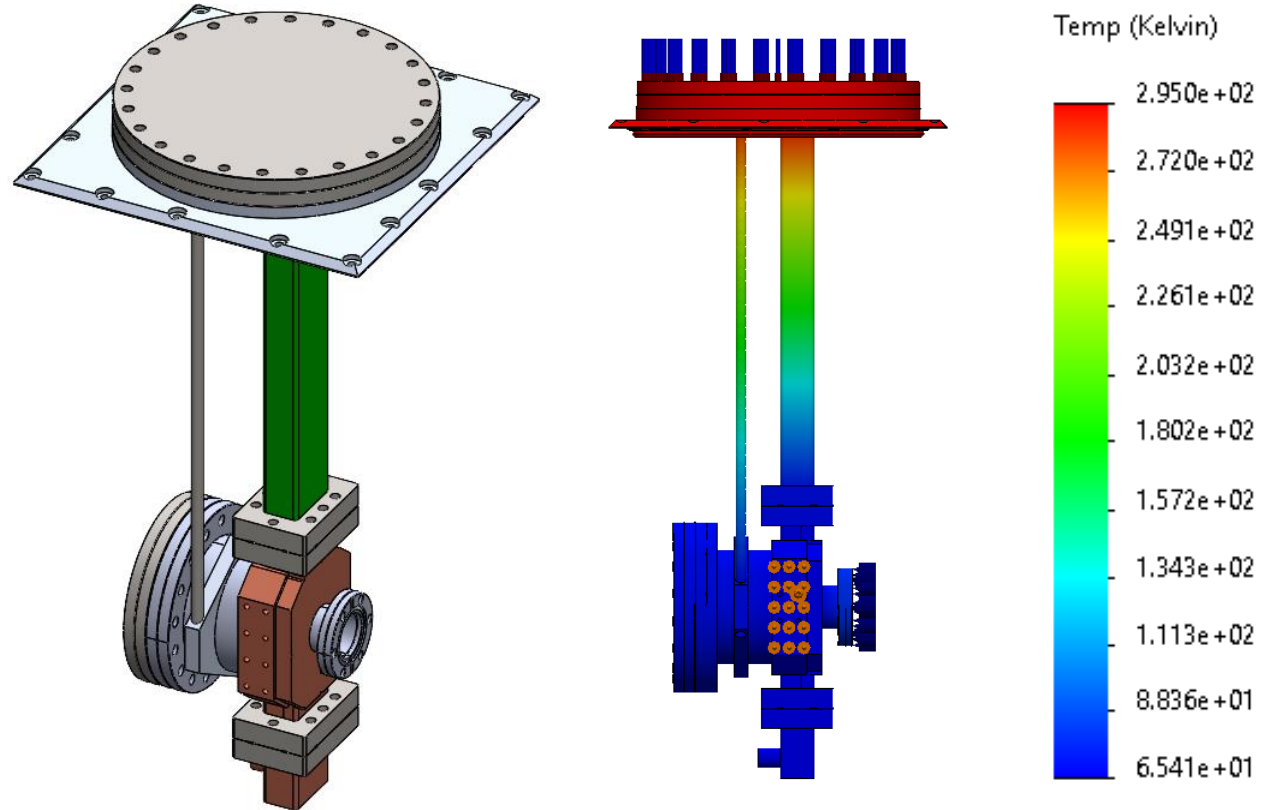


2) Steady State Thermal Sim



- Steady state thermal simulation results w/ 15W cooling from press fit with 3W heat leak budget

Description	Materials	Equivalent Area	Equivalent Power @ 65K	Equivalent Power @ 45K
Downstream CF flange	stainless, edge welded bellows	85 mm ²	4.8 W	5.2 W
Waveguide	Stainless	588 mm ²	6.6 W	7.1 W
Supports	Stainless + 2" G10	TBD	0.6 W	0.8 W
Diagnostic probes	Copper wiring	1.6 mm ²	≈ 0.1 W	≈ 0.1 W
Radiation	-	25000 mm ²	< 0.1 W	< 0.1 W
Pumping on dummy side	TBD	TBD	TBD	TBD
Upstream load lock	TBD	TBD	TBD	TBD
1Hz pulse heating	-	TBD	≈ 0.1 W	≈ 0.1 W





3) Pulse Heating

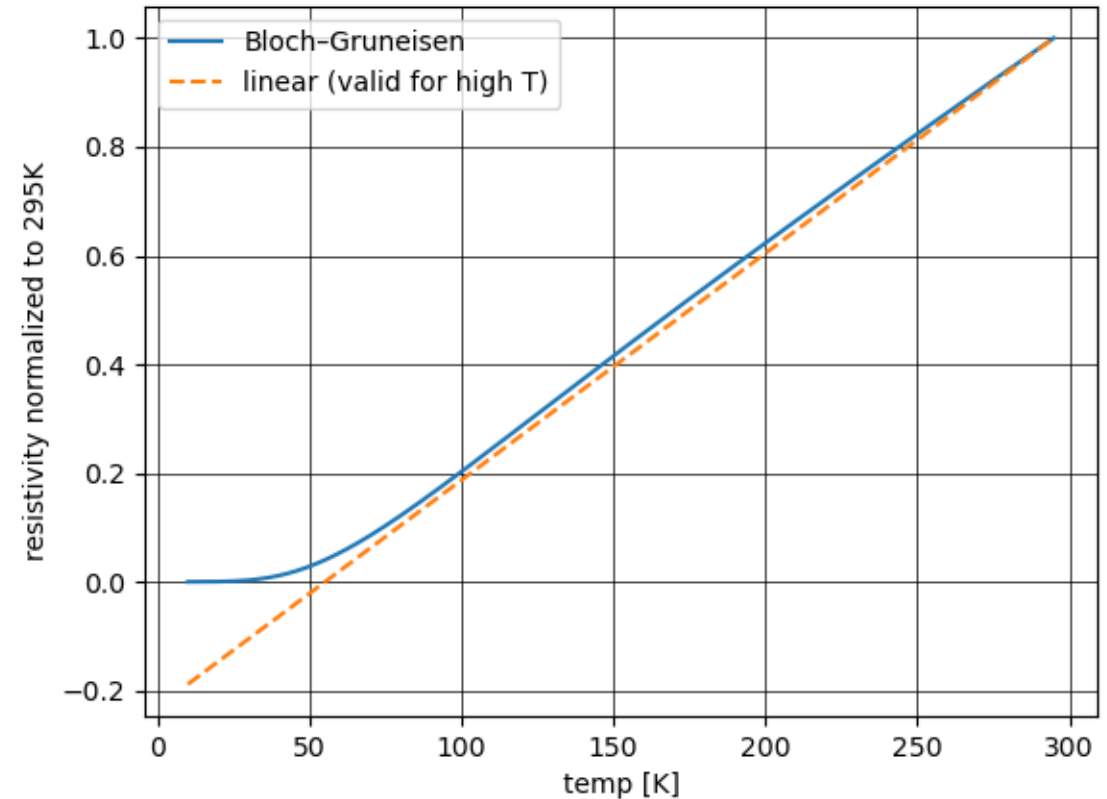


- Application to cryogenics worth working through similar RF pulsed heating calculation from Pritzkau (below)
- valid for linear bulk resistivity (also below)
 - Pritzkau linear model used for dashed curve previously (right)

$$\rho_{res}(T) = 7.012 \times 10^{-11}T - 3.865 \times 10^{-9} (\Omega \cdot m), \quad 273K \leq T \leq 800K$$

- bulk electric resistivity as function of temperature based on phonon model

$$\rho(T) = A \left(\frac{T}{\Theta_R} \right)^n \int_0^{\Theta_R/T} \frac{t^n}{(e^t - 1)(1 - e^{-t})} dt$$





3) Pulse Heating

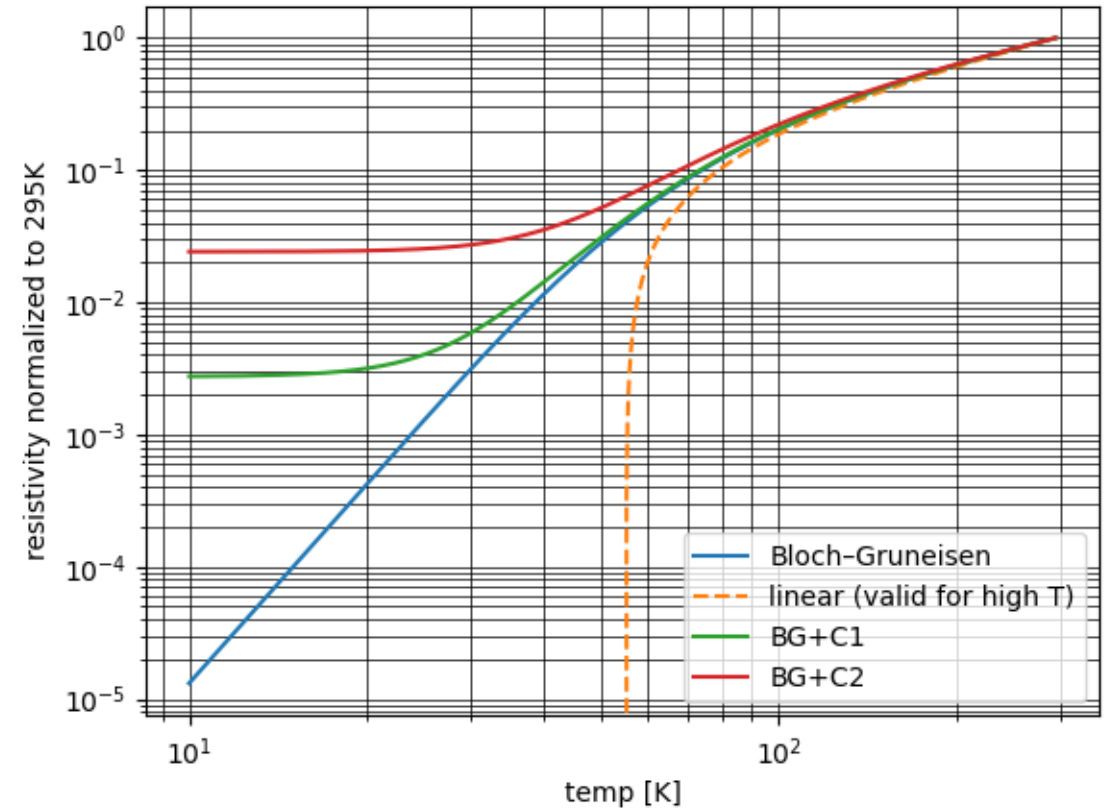


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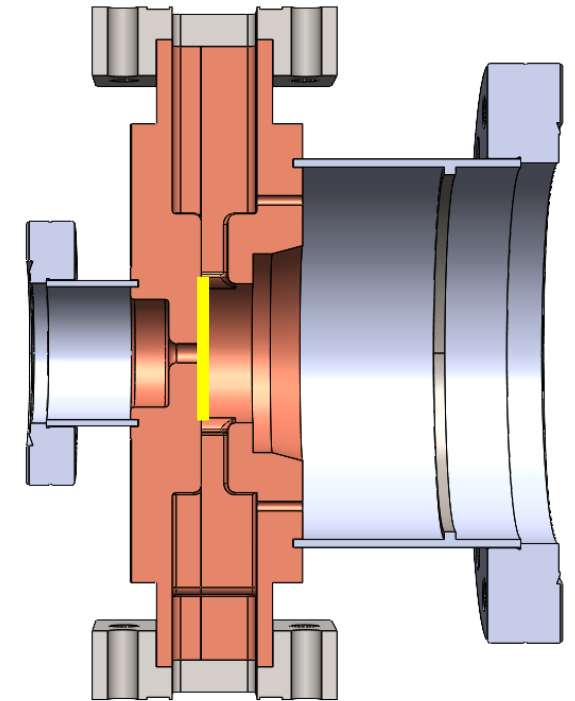
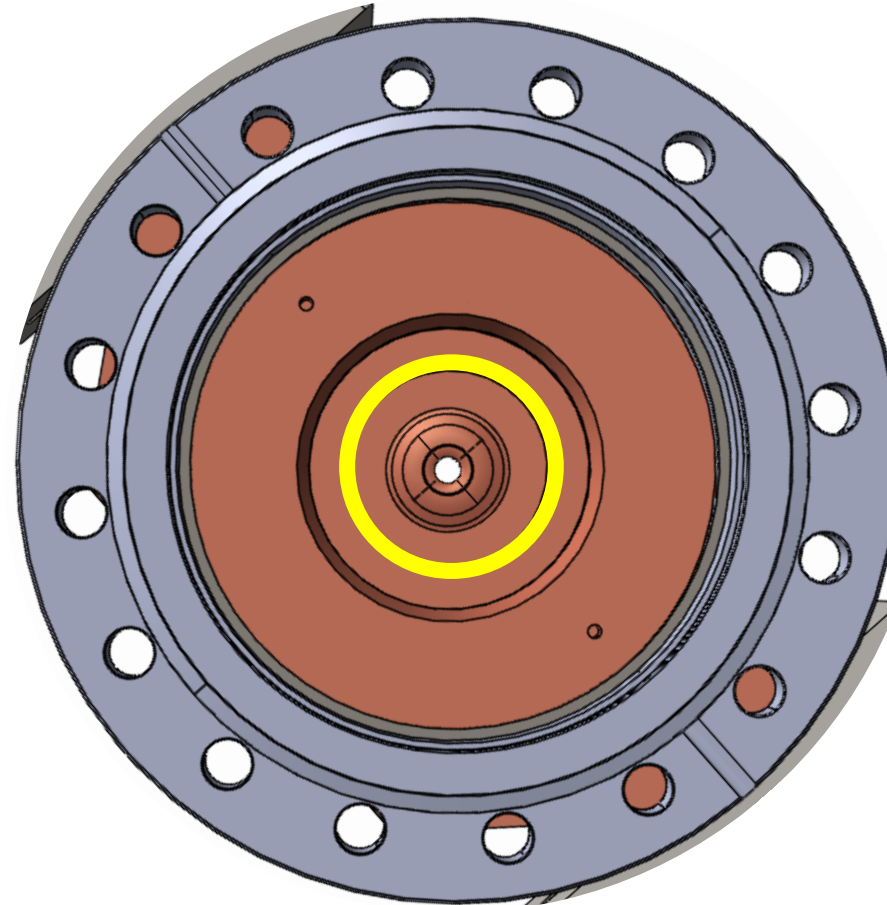
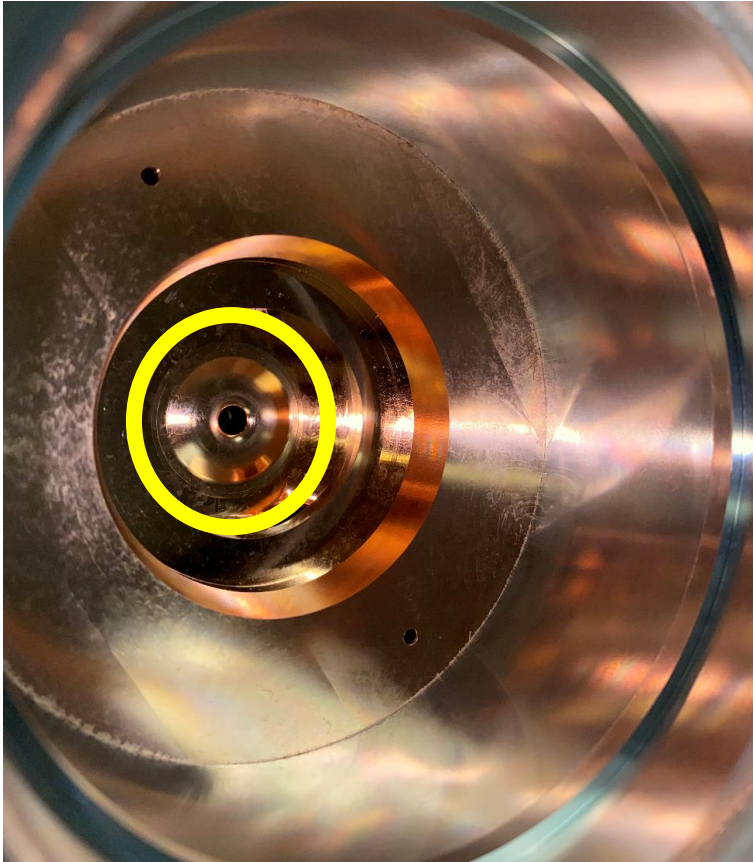
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3) Cavity faces



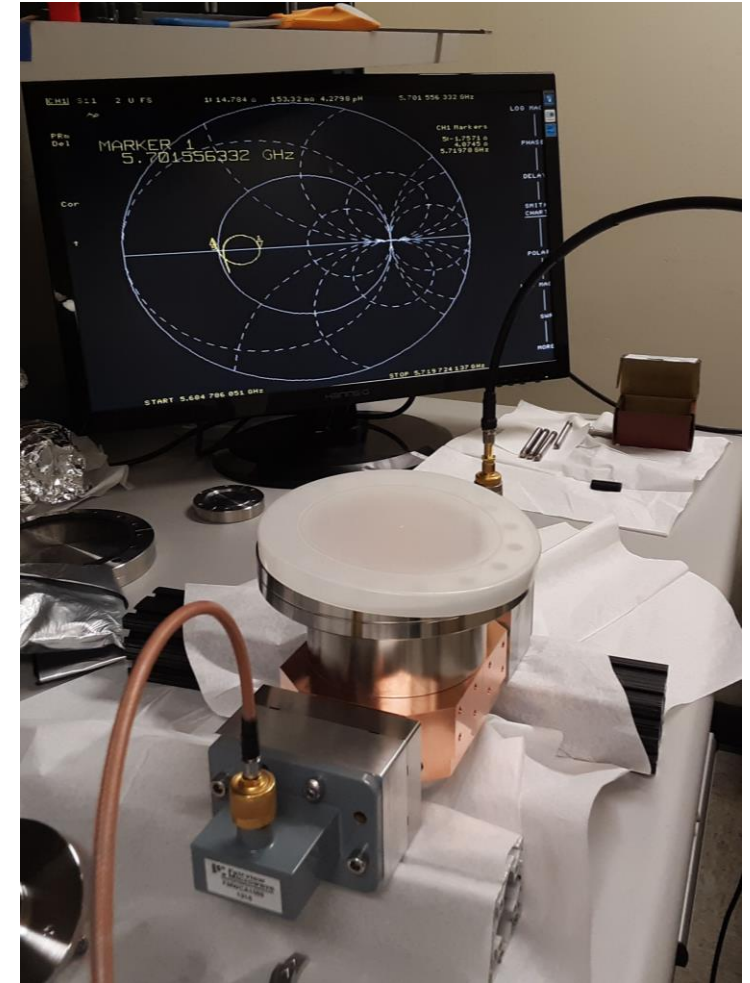
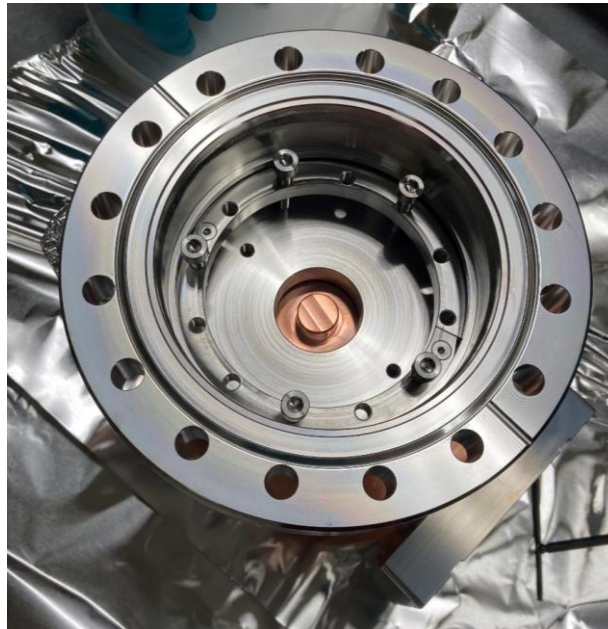


3) LLRF Measurements



- 295K resonance 6 MHz higher than intended and coupling lower
- Attributed to presence of braze material
- $Q_0 = 4200$ with no clamp, up to 7649 so far

	Measurement	Design/Simulation
f_0	5.701 GHz	5.695 GHz
β	0.52	0.7
QL	≈ 5000	5167
Q_0 (partial clamp)	≈ 4600	-
Q_0 (clamped)	7649	8579





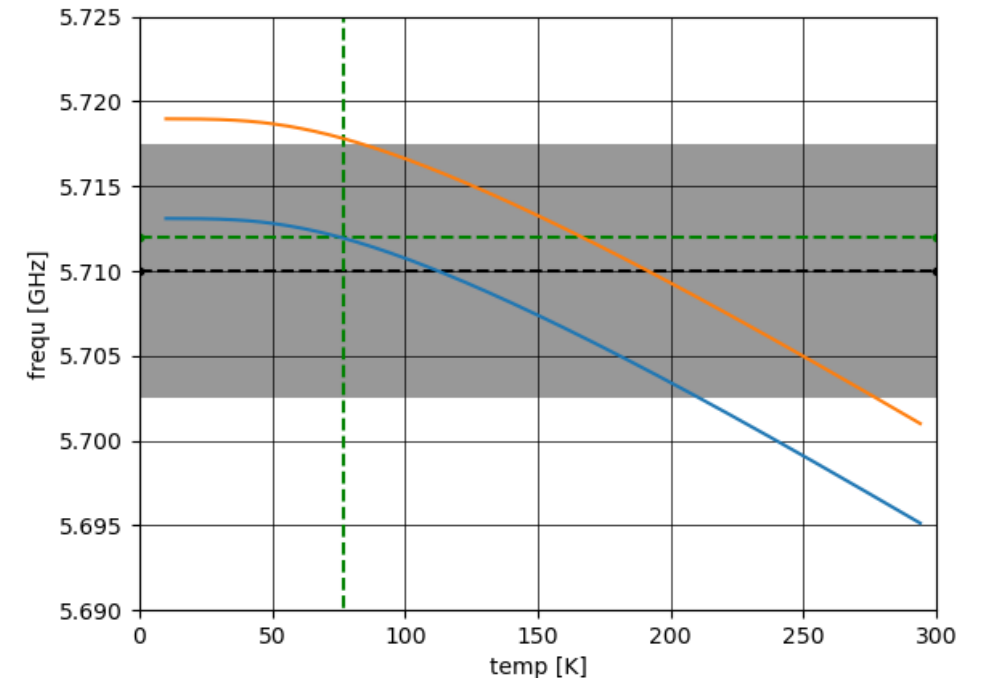
3) Cband RF Power



- 15 MHz bandwidth of klystron cryo outside range
- Verify bandwidth using new C-band mini-modulator

Parameter	100K
Launch field	120 MV/m
Frequency	5.711 GHz
β	3.1
Q0	18000
Filling time	0.25 us
RF Power requirement	0.56 MW
Energy deposition	0.22 J/pulse

Thales Klystron Bandwidth



Measurement w/ simulated cool down ———

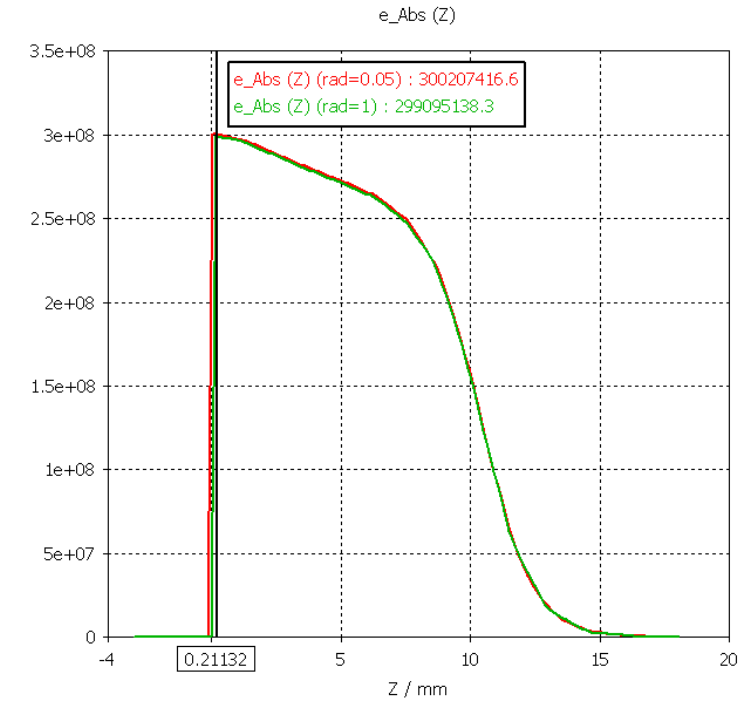
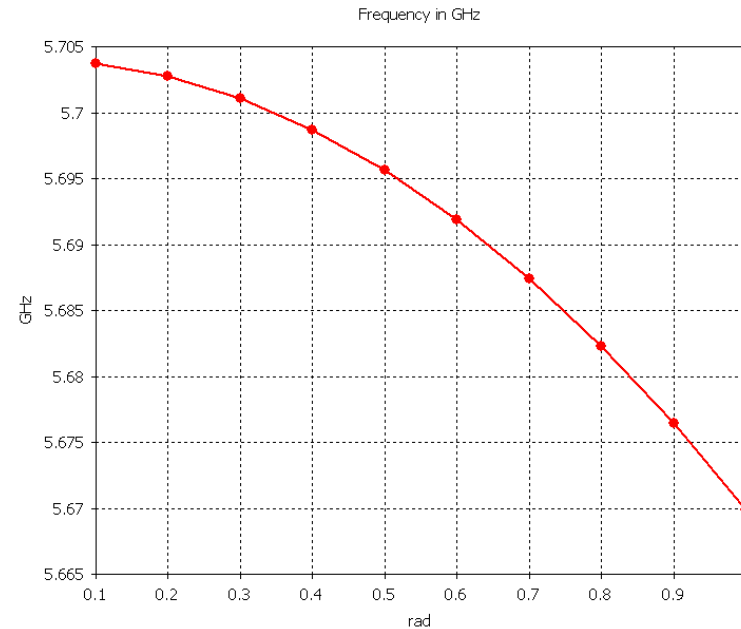
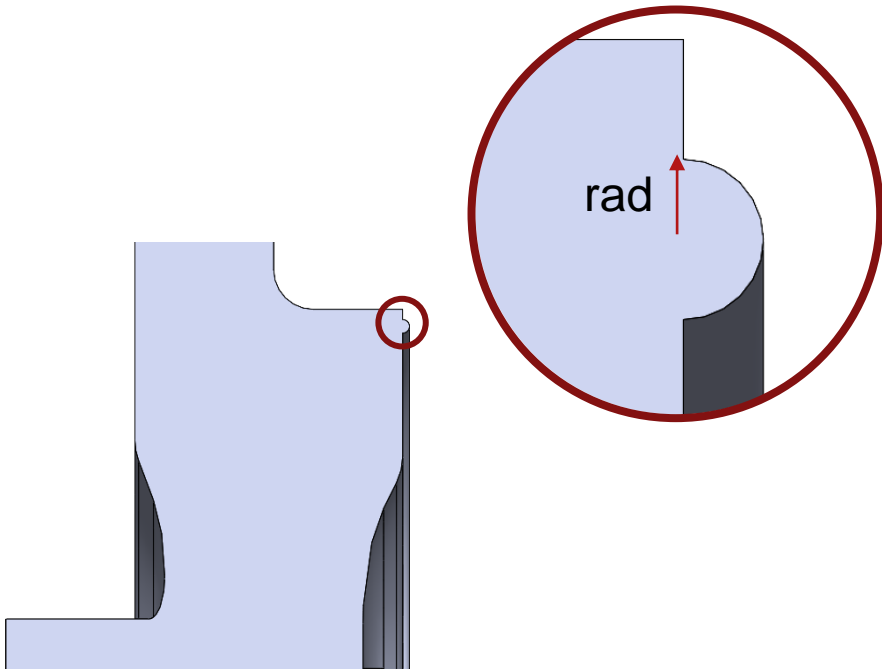
Design w/ simulated cool down ———



4) Backplane Modifications



1. Removal of material on backplane in high H, low E area on next backplane
2. Small hole for possible bead pull measurement
3. Optimization for acceptable cathode plug

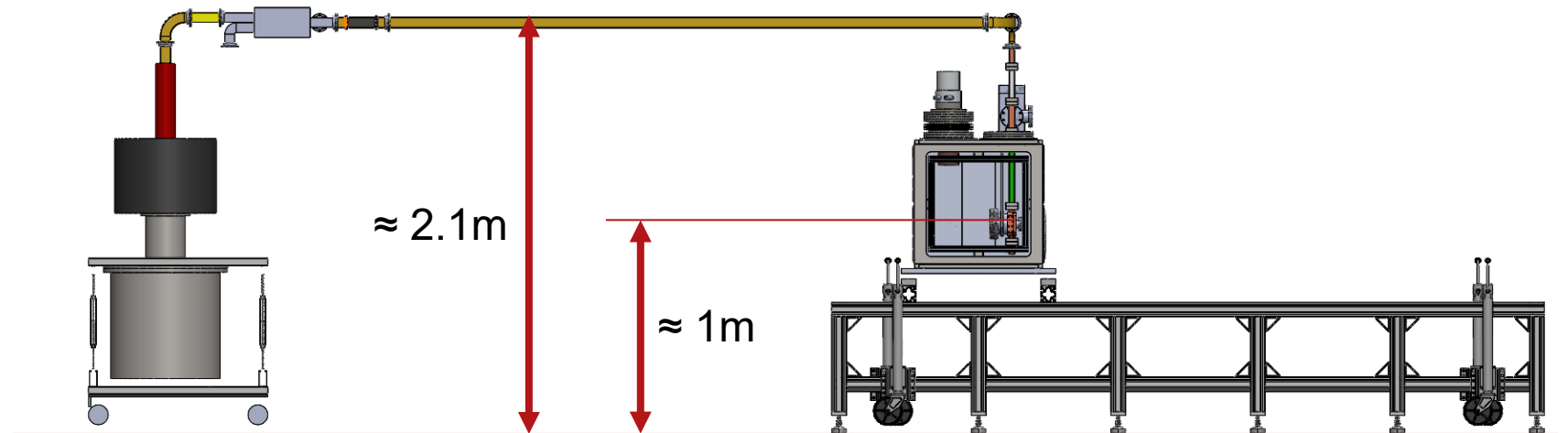
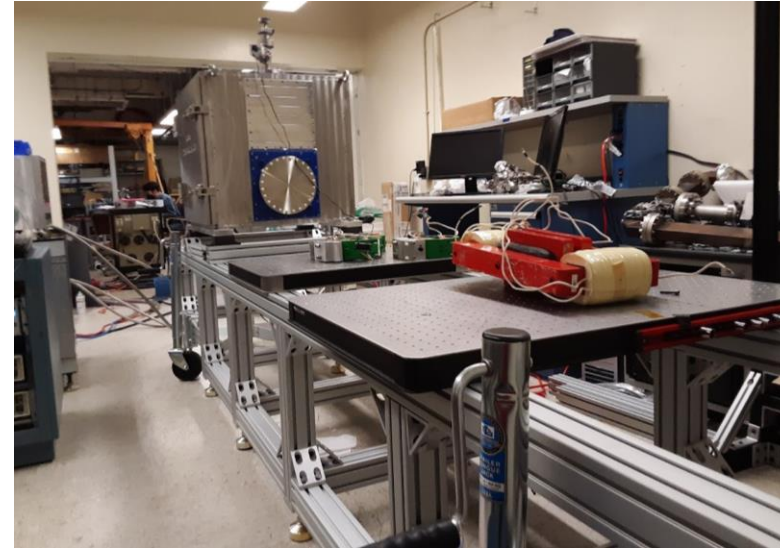




4) Phase1:config1



- Config 1 Goals:
 - LLRF (bead drop)
 - UHV test
 - cooldown & temperature stability
 - high power RF tests
 - Optimize RF pulse heating + cooling
 - SHI vibration isolation





5): Conclusions



1. CYBORG is part of planned high gradient cryogenic cathode test bed and stepping stone to high gradient cryogenic photoinjector
2. Preliminary LLRF tests begun & ongoing
3. Next steps are finishing infrastructure for high powered tests and beamline



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